PC1134 Lecture 23

Topic:

Divergence theorem and applications

Relevance:

- The divergence theorem converts a volume (triple) integral into a integral over a closed surface and vice versa. We can then evaluate whichever one is easier to do.
- Very important applications in electricity (Gauss' law), fluid dynamics (equation of continuity), heat flow, flow of particles, etc.

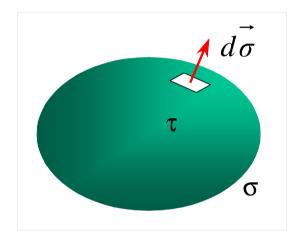
Scope

- The theorem
- Proof
- Equation of continuity
- Gauss's law
- Examples

Divergence Theorem

The normal surface integral of a function \vec{V} over the boundary of a closed surface of arbitrary shape is equal to the volume (triple) integral of the divergence of \vec{V} taken throughout the enclosed volume.

$$\iint\limits_{\sigma} \vec{V} \cdot d\vec{\sigma} = \iiint\limits_{\tau} \nabla \cdot \vec{V} d\tau$$



∬: integral over closed surface

d au: volume element

 $d\vec{\sigma}$: surface element

 $\mathsf{Magnitude} = \mathsf{area}$

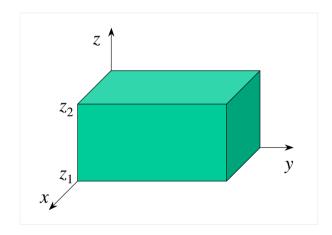
Direction: normal

Proof of Divergence Theorem

$$\iint_{\sigma} \vec{F} \cdot d\vec{\sigma} = \iiint_{\tau} \nabla \cdot \vec{F} d\tau$$

$$RHS = \iiint_{\sigma} \left(\frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z} \right) dx dy dz$$

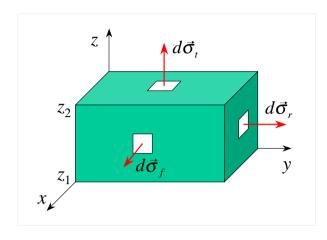
Consider the volume shown below



Integrate the last term with respect to z from z_1 to z_2

$$\iiint \frac{\partial F_z}{\partial z} dx dy dz = \iint_{\sigma} \left[F_z(x, y, z_2) - F_z(x, y, z_1) \right] dx dy$$
$$= \iint_{\sigma_t} F_z(x, y, z_2) dx dy - \iint_{\sigma_b} F_z(x, y, z_1) dx dy$$

Proof of Divergence Theorem (cont.)



$$\begin{array}{ll} \text{Bottom} & d\vec{\sigma}_b = -dxdy\hat{k} \\ \text{Front} & d\vec{\sigma}_f = dydz\hat{i} \\ \text{Left} & d\vec{\sigma}_l = -dzdx\hat{j} \\ \text{Top} & d\vec{\sigma}_t = dxdy\hat{k} \\ \text{Back} & d\vec{\sigma}_{bk} = -dydz\hat{i} \\ \text{Right} & d\vec{\sigma}_r = dzdx\hat{j} \end{array}$$

$$\hat{k} \cdot d\vec{\sigma}_t = dxdy$$

$$\hat{k} \cdot d\vec{\sigma}_b = -dxdy$$

$$\iiint \frac{\partial F_z}{\partial z} dx dy dz$$

$$= \iint_{\sigma_t} F_z(x, y, z_2) \hat{k} \cdot d\vec{\sigma}_t + \iint_{\sigma_b} F_z(x, y, z_1) \hat{k} \cdot d\vec{\sigma}_b$$

For all other surfaces (sides): $\hat{k} \cdot d\vec{\sigma} = 0$

$$\iiint \frac{\partial F_z}{\partial z} dx dy dz = \iint_{\sigma} F_z(x, y, z) \hat{k} \cdot d\vec{\sigma}$$

Proof of Divergence Theorem (cont.)

Similar integrations can be done to get

$$\iiint \frac{\partial F_x}{\partial x} dx dy dz = \iint_{\sigma} F_x(x, y, z) \hat{i} \cdot d\vec{\sigma}$$

$$\iiint \frac{\partial F_y}{\partial y} dx dy dz = \iint_{\sigma} F_y(x, y, z) \hat{j} \cdot d\vec{\sigma}$$

$$\iiint \frac{\partial F_z}{\partial z} dx dy dz = \iint_{\sigma} F_z(x, y, z) \hat{k} \cdot d\vec{\sigma}$$

Combine the three equations

$$\iiint \left(\frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} + \frac{\partial F_z}{\partial z}\right) dx dy dz$$

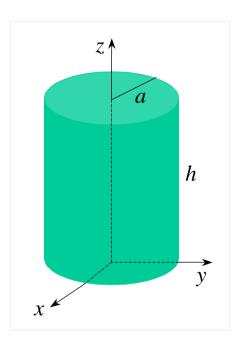
$$= \iint_{\sigma} \left(F_x \hat{i} + F_y \hat{j} + F_z \hat{k}\right) \cdot d\vec{\sigma}$$

Therefore

$$\iiint_{\tau} \nabla \cdot \vec{F} d\tau = \iint_{\sigma} \vec{F} \cdot d\vec{\sigma}$$

Example

Let $\vec{V}=x\hat{i}+y\hat{j}+z\hat{k}$, evaluate $\iint \vec{V}\cdot d\vec{\sigma}$ over the closed surface of the cylinder shown below.



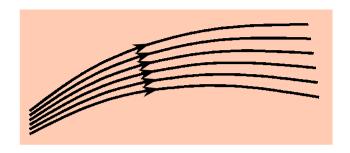
$$\iint_{\sigma} \vec{V} \cdot d\vec{\sigma} = \iiint_{\tau} \nabla \cdot \vec{V} d au$$
 $\vec{V} = x\hat{i} + y\hat{j} + z\hat{k}$
 $\nabla \cdot \vec{V} = 1 + 1 + 1 = 3$

$$\iint\limits_{\sigma} \vec{V} \cdot d\vec{\sigma} = \iiint\limits_{\tau} \nabla \cdot \vec{V} d\tau = 3 \iiint\limits_{\tau} d\tau = 3\pi a^2 h$$

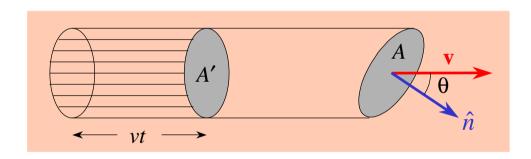
Flow of Substance

Water, gas, heat, radioactive particles, electric and magnetic fields, etc.

Stream line:



Assume density of fluid is ρ , velocity of fluid is \vec{v} .



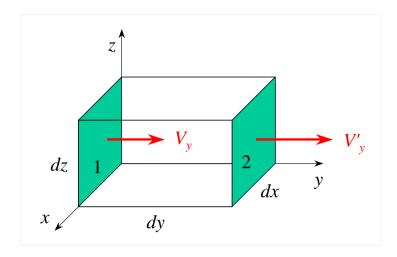
Amount of fluid crossing an area A' in time t is

$$egin{array}{ll} (vt)A'
ho & ec{v} ext{ is } \perp ext{ cross section} \ (vt)A
ho\cos\theta & ec{v}\cdot\hat{n}=v\cos\theta \ \end{array}$$

Amount of fluid cross unit area of the surface in unit time is

$$v\rho\cos\theta = V\cos\theta = \vec{V}\cdot\hat{n} \quad (V = \rho v)$$

Physical Meaning of Divergence



Assume that fluid flows from left to right and enters the left surface with velocity V_y and leaves the right surface with velocity V_y' . Amount of fluid flow into the volume through surface 1 is

$$(\vec{V} \cdot \hat{j})dxdz = V_y dxdz$$

Amount of fluid flow out of the volume through surface 2 is

$$V_y'dxdz = \left(V_y + \frac{\partial V_y}{\partial y}dy\right)dxdz$$

Net increase in mass

$$V_y dx dz - \left(V_y + \frac{\partial V_y}{\partial y} dy\right) dx dz = -\frac{\partial V_y}{\partial y} dx dy dz$$

Physical Meaning of Divergence (cont.)

Similarly, net mass increase due to flow in the x-direction and the z-direction are

$$-\frac{\partial A_x}{\partial x}dxdydz$$
, & $-\frac{\partial A_z}{\partial z}dxdydz$.

respectively. Total increase in mass per unit volume per unit time is

$$\begin{split} &\frac{1}{dxdydz} \left(-\frac{\partial A_x}{\partial x} - \frac{\partial A_y}{\partial y} - \frac{\partial A_z}{\partial z} \right) dxdydz \\ &= -\left(\frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} \right) = -\nabla \cdot \vec{A} \end{split}$$

If there is no source in the volume, this must be equal to the increase of the fluid mass per unit time per unit volume — rate of density increase

$$-\nabla \cdot \vec{A} = \frac{\partial \rho}{\partial t}$$
$$\nabla \cdot \vec{A} + \frac{\partial \rho}{\partial t} = 0$$

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(Equation of continuity)

Gauss' Law

Electric field: \vec{E}

Maxwell's equation: $abla \cdot ec{E} =
ho/arepsilon_0$

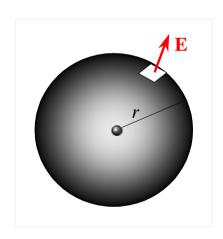
 ρ : charge density

 ε_0 : constant

$$\iint\limits_{\sigma} \vec{E} \cdot d\vec{\sigma} = \iiint\limits_{\tau} \nabla \cdot \vec{E} d\tau = \frac{1}{\varepsilon_0} \iiint\limits_{\tau} \rho d\tau$$
$$\iint\limits_{\sigma} \vec{E} \cdot d\vec{\sigma} = \frac{Q}{\varepsilon_0}$$

 $Q = \iiint_{\tau} \rho d\tau$ is the total charge inside σ .

Point Charge



$$\iint_{\sigma} \vec{E} \cdot d\vec{\sigma} = \iint_{\sigma} E d\sigma$$

$$= E \iint_{\sigma} d\sigma = 4\pi r^{2} E = \frac{Q}{\varepsilon_{0}}$$

$$E = \frac{Q}{4\pi\varepsilon_{0}} \frac{1}{r^{2}}$$